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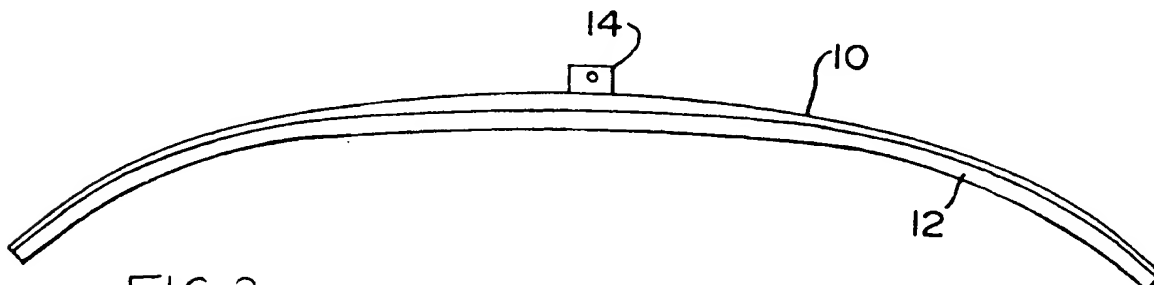
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(54) **Windscreen wiper.**

(57) A curved elongate backbone (10) for a windscreen wiper has a loading profile that increases substantially from a central connector (14) towards one or both ends of the backbone. The second differential of the bending moment also increases substantially from the connector towards the ends. The loading may increase right to the ends of the backbone or the backbone may have end portions with constant loading. In order to obtain the desired loading profile the width, thickness, and free-form radius of curvature are suitably selected. In preferred embodiments, the backbone (10) has a rectangular cross-sectional profile and the thickness and width decrease uniformly from the connector (14) to the ends. However, the thickness may also be constant for end portions.



**FIG 2**

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**THIS INVENTION** relates to a windscreen wiper and more particularly to an elongate curved backbone for a windscreen wiper which is of a suitably resiliently flexible material.

According to the invention there is provided a windscreen wiper which includes

- an elongate curved backbone which is of a resiliently flexible material and which has a connecting formation at a position intermediate its length for connection to a displacing and force applying member,
- the backbone having a suitably varying transverse cross-sectional profile along its length and a suitable free-form curvature for the backbone to achieve, when it is pressed downwardly at the connecting formation onto a flat surface by a force sufficient to straighten the backbone, a force per unit length exerted perpendicularly to the surface which increases substantially from the position of the connecting formation towards at least one end of the backbone.

The backbone may be curved in a plane- the plane of curvature.

Further according to the invention there is provided a windscreen wiper which includes

- an elongate backbone which is curved in a plane, which is of a resiliently flexible material and which has a connecting formation at a position intermediate its length for connection to a displacing and force applying member, the backbone having a suitably varying cross-sectional profile along its length and a suitable free-form curvature, such that the second differential of the function  $M(x)$  increases substantially from the said position towards at least one end of the backbone, where

$$M(x) = \frac{E * I(x)}{R(x)}$$

- with  $E$  = modulus of elasticity

$I(x)$  = cross-section moment of inertia of the backbone about a neutral axis transverse to the plane of curvature, at a distance  $x$  from the said position; and

$R(x)$  = free-form radius of curvature of the backbone in the plane of curvature at  $x$ .

- The wiper may include a wiper blade attached to the backbone and the sufficient force referred to above may be that force which causes the blade to contact the surface in a straight operative manner.

Persons skilled in the art will appreciate that the backbone will have a concave side and a convex side, the wiper blade being attached to the concave side and the displacing and force applying member on the convex side.

- The backbone may conveniently be of a metal such as spring steel and may be in the form of a single strip or may be in the form of a laminate.

- The connecting formation may be centrally located or the wiper may be asymmetric. The force per unit length may increase towards only one end of the backbone, but preferably it increases towards both ends of the backbone. Further, the force per unit length may increase towards both ends in a similar or dissimilar manner. Similarly, the second differential of  $M(x)$  may increase substantially from the connecting formation towards only one end or towards both ends. If it increases towards both ends this may be in a substantially similar or dissimilar manner.

- The force per unit length and the second differential of  $M(x)$  may increase progressively towards the ends of the backbone until a short distance from each end and the backbone may then have two small portions at each end where the force per unit length and the second differential are a constant value. Further, the backbone may be such that in these small portions the force per unit length and the second differential are constant right to the tips of the backbone, or, at tip regions the backbone may be such that the force per unit length and the second differential decrease from the constant value to zero at the extremities of the backbone.

The force per unit length may increase, at least in the central region of the backbone, in an exponential manner. Conveniently,

$$f(x) = A|x|^n + C$$

where

$f(x)$  = force per unit length at a distance  $x$  from the connecting formation,

$A$  and  $C$  are determinable constants, and

$n$  is greater than unity.

- Conveniently,  $n$  may be at least 3, is generally at least 6 and is preferably about 10.

- Those skilled in the art will appreciate that  $I(x)$  is determined by the transverse dimensions of the backbone at any position along its length. In most cases, the backbone will have a regular cross-sectional profile which may, for example be rectangular or ellipsoidal. Thus, in most instances, the backbone will have a width and a thickness. It will be understood that the width dimension will be that dimension which extends perpendicularly to the plane of curvature and the thickness will be the dimension which lies in the plane of curvature.

The thickness of the backbone may decrease from the connecting formation towards both ends until a predetermined distance from the ends, with the thickness being constant along these end portions. These end portions may have a length of at least 20 mm.

It can be shown, that with a backbone which has a rectilinear cross-section at all positions along its length, that

$$M(x) = \frac{E * b_x * h_x^3}{12 * R_x}$$

5 where

$b_x$  equals the width at distance  $x$ ,

$h_x$  equals thickness at distance  $x$ .

Thus, with a backbone having a rectangular cross-section, the width and thickness may vary in a predetermined manner and the radius of curvature may then be varied so that  $M(x)$ , and its second differential vary in the desired manner.

10 If the backbone has an elliptical cross-section then it can be shown that

$$M(x) = \frac{\pi * E * b_x * h_x^3}{64 * R_x}$$

15 If the backbone has any other cross-sectional profile the equation for  $M(x)$  may be determined utilising conventional mathematical techniques.

Those skilled in the art will appreciate that there is a relationship between the second differential of  $M(x)$  and the force per unit length. Thus, the second differential of  $M(x)$  may vary in the same manner as that described above for the force per unit length.

20 It will be appreciated further that the width, thickness and radius of curvature also determine other characteristics of the backbone. Thus, the radius of curvature of the backbone will determine the extent of curvature of a windscreen that can be cleaned by the wiper. Thus, if the windscreen, in any particular region, has a greater curvature than that portion of the wiper that is to pass thereover, then the wiper will not clean that region of the windscreen in an effective manner.

25 Similarly, the width and thickness will determine the rigidity of the wiper and if the backbone is too thin at its tips it will be vulnerable to mechanical damage.

Those skilled in the art will also appreciate that  $M(x)$  is the bending moment of the backbone.

Further, if a curved beam is uniformly loaded, ie. the force per unit length is a constant along the length of the beam when it is pressed down onto a flat surface, then the bending moment is

$$30 \quad M_c(x) = \frac{F * (4x^2 - 4Lx + L^2)}{8 * L}$$

where

$F$  = the total force applied to the beam to straighten it against a flat surface, and

$L$  = the length of the beam.

Thus, with a rectilinear backbone if

$$35 \quad \frac{b_x * h_x^3}{R_x} > \frac{12 * F * (4x^2 - 4Lx + L^2)}{8 * L * E}$$

at all positions along at least a part of the backbone (which is a substantial part), then the backbone will be such that the force per unit length increases along the length of this part of the backbone away from the connecting formation.

40 Similarly, with an elliptical cross-section, the backbone will have an increasing force per unit length if

$$\frac{b_x * h_x^3}{R_x} > \frac{8 * F * (4x^2 - 4Lx + L^2)}{\pi * E * L}$$

For practical reasons, the backbone should have end portions with a constant radius of curvature, and the tips themselves are preferably straight.

45 The invention is now described by way of example only with reference to the drawings in which:

Figure 1 is a perspective view from above of the windscreen wiper of the invention with the drawing being shortened for clarity of illustration;

Figure 2 is a side elevation of the Figure 1 windscreen wiper shown in an unloaded free form condition;

50 Figure 3 is an end elevation of the wiper;

Figure 4 is a force distribution diagram illustrating the lengthwise distribution of the force per unit length on the windscreen wiper of Figures 1 to 3 when it is pressed against a flat surface in an operational manner; Figure 5 illustrates the curvature requirement to which a wiper blade should conform to operate satisfactorily on a typically curved motor vehicle windscreen;

55 Figure 6 shows graphically the variation in the radius of curvature of the wiper of Figures 1 and 2 in its free form condition;

Figure 7 shows graphically the variation in the radius of curvature of a further embodiment of a wiper which has a symmetrical backbone with tip portions of constant thickness; and

Figure 8 shows graphically the variation in the radius of curvature of a still further embodiment of a wiper which has an asymmetric backbone with tip portions of constant thickness.

The windscreen wiper of the invention is shown in Figures 1 to 3 to include a spring backbone 10 and a wiper blade 12. The backbone 10 has a centrally located connector 14 for releasably connecting the wiper to a spring loaded wiper arm (not shown). The connector 14 could be of any suitable type. The backbone 10 has suitable attachment formations (also not shown) to ensure that the blade 12 is securely attached to the backbone 10.

The spring backbone of the wiper is preferably made from spring steel and tapers both in width and thickness from its centre towards its free ends or tips. The backbone is pre-curved longitudinally with a predetermined radius of curvature at every point in its length. The backbone 10 defines a plane, which is defined by the sheet of paper in Figure 2. The cross section of the backbone is preferably rectangular but may be of any other suitable shape. Most importantly to the invention the thickness and width of the backbone 10 and its radius of curvature are matched at every point along the length of the backbone so that the backbone will provide a force per unit length distribution in a longitudinal direction which increases towards both tips of the windscreen wiper when the windscreen wiper is, in use, pressed downward intermediate its ends onto a flat surface, as shown in Figure 1, by a force F which is equal in magnitude to the down force required to straighten the backbone. By straighten is meant that the force F must be adequate to render the wiper blade 12 fully functional.

A suitable force per unit length distribution is shown in Figure 4, where the various parameters have the following meaning:

F = downforce applied to wiper by wiper arm.  
 $f(x)$  = force per unit length distribution between  $-X_{LMAX}$  and  $X_{LMAX}$  in N/m.  
 B = Maximum loading acceptable at tips, in N/m.  
 $X_{LMAX}$  = point where maximum loading starts.  
 $D_{X_{LMAX}}$  = distance from tip for which the maximum loading B applies  
 L = length of wiper blade.

In this example, the following values are assumed:-

F = 6,975 N  
 L = 0,45 m  
 $D_{X_{LMAX}}$  = 0,02 m, therefore  $X_{LMAX} = 0,205$  m  
 B = 34,1 N/M

It will be appreciated that the distribution between  $-X_{LMAX}$  and  $+X_{LMAX}$  is of the form

$$f(x) = A |x|^n + C \quad (1)$$

where

$n = 10$ .

The co-efficient A in equation (1) is determined from the formula

$$A = \frac{(n + 1) [F - 2Cx_{LMAX} - 2B D_{X_{LMAX}}]}{2 X_{LMAX}^{n+1}} \quad (2)$$

Equation (2) represents a situation where the force distribution balances the total force F. As indicated in the broad description above, the distribution at the ends of the backbone is a constant (B). Further, as indicated above, the loading may decrease right at the tips, although this is not shown in Figure 4.

To achieve the increasing loading (as discussed above) the thickness of the spring backbone at any position in its length must subscribe to the following equation:

$$h(x) > \left[ \frac{3R_x F (4x^2 - 4Lx + L^2)}{2LEb_x} \right]^{1/3}$$

The above equation relates to a wiper backbone which has a substantially rectangular cross sectional shape. In further experimentation with the wiper backbone of the invention it may, however, as mentioned above, be found that cross sectional shapes other than rectangular may provide the backbone with better

structural characteristics than does the rectangular backbone. In this event, the equation will need to be adapted to suit the particular shape required. For example, in a backbone having an elliptical cross section the equation will need to be adjusted as follows:

$$h(x) > \left[ \frac{8R_x F (4x^2 - 4Lx + L^2)}{\pi L E b_x} \right]^{1/3}$$

The wiper blade 12 is made from a suitable rubber or elastomeric material and in the currently preferred embodiment of the invention is shaped in cross section as illustrated in Figure 3. The cross sectional shape of the blade 12 may, however, if required, be made variable at various positions in its length.

#### EXAMPLE 1

A wiper backbone, which is of spring steel and has a rectangular cross-sectional profile and which has the required loading increase towards its tips, torsional rigidity and wrap around capability has the following dimensional values:

modulus of elasticity

$$= 207 \text{ GPa} \quad 207 \times 10^9 \text{ N/m}^2 \text{ PA}$$

length

450 mm

thickness at the centre of the backbone 1,29 mm

thickness at the tips

0,22 mm

width at the centre

11 mm

width at the tips

6 mm

$$1 \text{ Pa} = 1 \times 10^{-9} \text{ BA}$$

The backbone tapers uniformly in both thickness and width in a straight line manner from its centre to its tips.

As has been mentioned above it is essential to this invention that the reactive loading on the wiper backbone when pressed onto a flat surface, as illustrated in Figure 4, must increase towards the tips of the backbone as shown in the drawing.

The curvature required to give this loading profile is determined in the following way.

Using equation (1) above, the parameter C in Figure 4 is calculated iteratively until  $f(x) = B$  at the point

$$X = X_{LMAX}$$

In this example,

$$C = 11,64 \text{ N/m.}$$

With C known, A can now be determined from equation (2). The value of A is approximately 171 300 000 N/m<sup>11</sup>.

From basic Strengths of Material theory, the bending moment equation where  $L/2 > |x| > X_{LMAX}$  is

$$M(x) = \frac{1}{2} B [X^2 - L|x| + L^2/4] \quad (3)$$

By derivation from Standard Strengths of Material theory, the bending moment equation where  $X < X_{LMAX}$  is

$$m(X) = A \left\{ \frac{1}{n+1} - \frac{1}{n+2} \right\} x^{n+2} + \frac{C}{2} x^2 - \left\{ \frac{AY^{n+1}}{n+1} + CY \right\} x + \left\{ \frac{CY^2}{2} + \frac{AY^{n+2}}{n+2} \right\} + \frac{B}{2} \left\{ Y(2x - Y) - Lx + \frac{L^2}{4} \right\} \quad (4)$$

where  $Y = X_{LMAX}$

$$\begin{aligned} W &= 19.7 \\ R &= -1.15 \times 10^{-2} \\ t &= 1.12 \text{ mm} \end{aligned}$$

At any point  $x$  along the length of the backbone, the radius of curvature  $R$  is given by

$$R(x) = \frac{EI(x)}{M(x)} \quad (5)$$

where  $I(x)$  = cross section moment of inertia at position  $x$ ,

5  $E$  = modulus of elasticity (Young's modulus)

$M(x)$  = is given by either equation (3) or (4), depending on the value of  $x$ .

Using equation (5) the radius of curvature as shown in Figure 6 is determined.

At all points  $x$  (except for the last 45 mm at the tips) the example backbone satisfies the curvature requirements represented by Figure 5, ie.  $R(x)$  according to equation (5) is smaller than the required radius of curvature.

## EXAMPLE 2

The example described above is of a wiper having a rectangular backbone which tapers uniformly in both thickness and width in a straight line manner from its centre to its tips. As indicated above, the backbone could have tip portions of constant thickness. The dimensions and other values for such a backbone in accordance with the invention are:-

20	$F$	= 6,3 N
	$L$	= 44 cms
	$D_{XLMAX}$	= 3 cms, therefore
25	$X_{LMAX}$	= 19 cms
	$B$	= 20 N/m
30	$n$	= 10
	modulus of elasticity	= $207 \times 10^9 \text{ N/m}^2$
	length	= 440 mm
35	thickness at the centre of the backbone	= 1,15 mm
	thickness at the tip portions	= 0,43 mm
40	distance from the tips for which thickness remains constant	= 45 mm
	width at centre	= 11 mm
45	width at the tips	= 6 mm.

$W = 15.3.7$   
 $R = -1.185 \times 10^{-2}$   
 $b = 1.12$   
 $R_x = -4.4 \times 10^3$

Thus, the backbone tapers uniformly in width from its centre to its tips and uniformly in thickness from its centre to 175 mm from the centre, then the thickness remains constant for the next 45 mm right to the tips.

50 These parameters produce the following results:-

$$C = 12,85 \text{ N/m}$$

$$A = 102\,000\,000 \text{ N/m}^{11} \text{ (approximately).}$$

Using these values in equations (3), (4) and (5) above, the following radius of curvature are obtained:-

55

U 1 5 10  
 2 6 11  
 3 7 12  
 4 8 1  
 9 — 1  
 WACIN  
 VSC

	<u>X (cm)</u>	<u>Radius of Curvature (m)</u>
	0	0,766
5	2	0,704
	4	0,643
10	6	0,586
	8	0,535
	10	0,490
15	12	0,454
	14	0,430
20	16	0,433
	18	0,568
	20	2
25	22	826

The radius of curvature of such a wiper is shown graphically in Figure 7.

### 30 EXAMPLE 3

Further, as indicated above a rectangular backbone could be assymmetric, having a connector that is not centrally located, and the loading is different towards both ends. The dimensions of, and other values for, such a backbone in accordance with the invention are:-

35  $F = 6,3 \text{ N}$   
 $L = 45 \text{ cms.}$

The connection point is shifted 13 mm longitudinally from the geometric centre, to one side of the backbone. The shorter side of the backbone is therefore 212 mm long and the longer side is 238 mm long.

40 Dealing firstly with the shorter side. The total force applied to the shorter side of the beam is 3.2 N, therefore for a notional symmetric backbone

$$F = 2 * 3,2 \text{ N} = 6,4 \text{ N}$$

The length of the shorter side is 212 mm, therefore for a notional symmetric backbone

$$L = 2 * 212 \text{ mm} = 424 \text{ mm}$$

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	$D_{XLMAX}$	= 3cms, therefore
	$X_{LMAX}$	= 18.2 cms
5	B	= 22 N/m
	n	= 10
10	modulus of elasticity	= $207 \times 10^9$ N/m <sup>2</sup>
	thickness at connector	= 1,15 mm
	thickness at tips	= 0,43 mm
15	distance from the tips for which thickness remains the same	= 45 mm
20	width at connector	= 11 mm
	width at the tips	= 6 mm.

$$L = 424$$

Thus the shorter side of the backbone has a width that decreases uniformly to the tip and a thickness that decreases uniformly for a distance of 167 mm from the connector and which then remains constant for the remaining 45 mm right to the tip.

These parameters produce the following results for the short side of the blade:-

$$C = 13,1 \text{ N/m}$$

$$A = 236\,000\,000 \text{ N/m}^{11} \text{ (approximately).}$$

Using these above values in equations (3), (4) and (5) above, the following radii of curvature result:-

	<u>X (cm)</u>	<u>Radius of Curvature (m)</u>
35	0	0,778
	2	0,709
	4	0,641
40	6	0,579
	8	0,522
45	10	0,472
	12	0,433
	14	0,408
50	16	0,416
	18	0,777
55	20	4,657.

Dealing now with the longer side of the backbone.

The total force applied to the longer side of the backbone is 3,1 N, therefore for a notional symmetric back-



bone

$$F = 2 * 3.1 \text{ N} = 6.2 \text{ N}$$

The length of the longer side is 238 mm therefore for a notional symmetric backbone

5	$L$	$= 2 * 238 \text{ mm} = 476 \text{ mm}$
	$D_{XLMAX}$	$= 0, \text{ therefore}$
10	$X_{LMAX}$	$= 238 \text{ mm}$
	$B$	$= 13.1 \text{ N/m}$
	$n$	$= 10$
15	thickness at connector	$= 1.15 \text{ mm}$
	thickness at tips	$= 0.40 \text{ mm}$
20	distance from the tips for	
	which thickness remains the same	$= 45 \text{ mm}$
	width at connector	$= 11 \text{ mm}$
25	width at the tips	$= 6 \text{ mm}.$

Thus the longer side of the backbone has a width that decreases uniformly to the tip and a thickness that decreases uniformly from the connector for a distance of 193 mm and then remains constant for the next 45 mm right to the tip.

With this example, the longer side has uniform loading and thus, these parameters produce, for the longer side,

$$C = 13.1 \text{ N/m}$$

$$A = 0 \text{ N/m}^{11}; \text{ and}$$

Using the above values, as before, the following radii of curvature are obtained.

	<u>X (cm)</u>	<u>Radius of Curvature (m)</u>
	0	0,779
5	2	0,727
	4	0,675
10	6	0,627
	8	0,584
	10	0,546
15	12	0,515
	14	0,493
20	16	0,488
	18	0,515
	20	0,757
25	22	2.993.

The radius of curvature of such a wiper is shown graphically in Figure 8.

It will be noted that, with the first two examples, between  $-X_{LMAX}$  and  $X_{LMAX}$ , the force per unit length exerted perpendicularly when the backbone is straightened increases substantially from the middle towards the ends; the second differential of  $M(x)$  also increases substantially; and

$$\frac{b_x \cdot h_x^3}{R_x} > \frac{12 \cdot F(4x^2 - 4Lx + L^2)}{8 \cdot L \cdot E.}$$

at all positions. This is also the case with the shorter side of the third example.

The invention is not limited to the precise details as herein described. For example it is not essential that the backbone of the wiper tapers uniformly from the centre down towards the tips and in some applications the load distribution of the blade on the glass of a specific windshield may need to increase only towards one tip of the wiper. Additionally, as indicated above, to achieve a constant angle of wipe of the blade 12 along its length it may be necessary to shed the distributed blade load at the tip portions of the wiper.

## Claims

1. A windscreen wiper which includes  
an elongate curved backbone which is of a resiliently flexible material and which has a connecting formation at a position intermediate its length for connection to a displacing and force applying member; the backbone having a suitably varying transverse cross-sectional profile along its length and a suitable free-form curvature for the backbone to achieve, when it is pressed downwardly at the connecting formation onto a flat surface by a force sufficient to straighten the backbone, a force per unit length exerted perpendicularly to the surface which increases substantially from the position of the connecting formation towards at least one end of the backbone.
2. The wiper as claimed in Claim 1, in which the backbone is curved in a plane.
3. A windscreen wiper which includes  
an elongat backbone which is curved in a plane, which is of a resiliently flexible material and which has a connecting formation at a position intermediate its length for connection to a displacing and force applying member, the backbone having a suitably varying cross-sectional profile along its length and a

suitable free-form curvature such that the second differential of the function  $M(x)$  increases substantially from the said position towards at least one end of the backbone, where

$$M(x) = \frac{E * I(x)}{R(x)}$$

5 with  
 $E =$  the modulus of elasticity  
 $I(x) =$  the cross-section moment of inertia of the backbone about a neutral axis transverse to the plane of curvature, at a distance  $x$  from the said position; and  
 $R(x) =$  the free-form radius of curvature of the backbone in the plane of curvature at  $x$ .

- 10 4. The wiper claimed in claim 1, 2, or 3, including a wiper blade attached to the backbone.
5. The wiper claimed in any one of the preceding claims, in which the connecting formation is centrally located.
- 15 6. The wiper claimed in any one of Claims 1 to 4, in which the connecting formation is not centrally located.
7. The wiper claimed in any preceding claim, in which the perpendicularly exerted force per unit length increases substantially from the position of the connecting formation towards both ends of the backbone.
- 20 8. The wiper claimed in Claim 7, in which the force per unit length increases towards both ends in a substantially similar manner.
9. The wiper claimed in Claim 7, in which the force per unit length increases towards both ends in a dissimilar manner.
- 25 10. The wiper claimed in Claim 3, in which the second differential of  $M(x)$  increases substantially from the position of the connecting formation towards both ends of the backbone.
11. The wiper claimed in Claim 10, in which the second differential of  $M(x)$  increases towards both ends in a substantially similar manner.
- 30 12. The wiper claimed in Claim 10, in which the second differential of  $M(x)$  increases towards both ends in a dissimilar manner.
13. The wiper claimed in Claim 1 or 2, in which the force per unit length increases progressively towards at least one end of the backbone until a predetermined distance from the tip thereof and the force per unit length along this end portion is substantially constant.
- 35 14. The wiper claimed in Claim 3, in which the second differential of  $M(x)$  increases progressively towards at least one end of the backbone until a predetermined distance from the tip thereof and the second differential of  $M(x)$  along this end portion is substantially constant.
- 40 15. The wiper claimed in any one of Claims 1, 2, 7, 8, 9, 13 or 14 in which the force per unit length increases, in at least a central region of the backbone in an exponential manner.

- 45 16. The wiper claimed in Claim 15, in which

$$f(x) = A |x|^n + C$$

where

$f(x)$  = force per unit length at a distance  $x$  from the connecting formation;

$A$  and  $C$  are determinable constants; and

$n$  is greater than unity.

- 50 17. The wiper claimed in Claim 3, in which the second differential of  $M(x)$  increases in an exponential manner.

18. The wiper claimed in Claim 17, in which  $M''(x) = A |x|^n + C$

where

$M''(x)$  is the second differential of  $M(x)$ ;

$A$  and  $C$  are determinable constants; and

$n$  is greater than unity.

19. The wiper claimed in Claim 16 or 18, in which  $n$  is about 3 or greater than 3, preferably about 6 or greater than 6, and more preferably about 10 or greater than 10.

20. The wiper claimed in any one of the preceding claims in which the backbone has a thickness dimension  $h$  which varies from the position of the connecting formation towards at least one end of the backbone until a predetermined distance from the said end and which is constant along said end portion, which preferably has a length of at least 20 mm.

21. A windscreen wiper which includes

an elongate backbone which is curved in a plane, which is of a resiliently flexible material and which has a connecting formation at a position intermediate its length for connection to a displacing and force applying member;

the backbone having a rectilinear transverse cross-sectional profile along a substantial part of its length and in which, at all positions along said part

$$\frac{b_x \cdot h_x^3}{R_x} > \frac{12 \cdot F(4x^2 - 4Lx + L^2)}{8 \cdot L \cdot E}$$

where

$b_x$  = width at distance  $x$  from the connection formation;

$h_x$  = thickness at  $x$ ;

$R_x$  = free-form radius of curvature of the backbone in the plane at  $x$ ;

$F$  = the total force applied to the said part of the backbone to straighten it against a flat surface;

$L$  = the length of said part; and

$E$  = modulus of elasticity.

22. A windscreen wiper which includes

an elongate backbone which is curved in a plane, which is of a resiliently flexible material and which has a connecting formation at a position intermediate its length for connection to a displacing and force applying member;

the backbone having an elliptical transverse cross-sectional profile along a substantial part of its length and in which, at all positions along said part

$$\frac{b_x \cdot h_x^3}{R_x} > \frac{8 \cdot F(4x^2 - 4Lx + L^2)}{\pi \cdot E \cdot L}$$

where

$b_x$  = width at distance  $x$  from the connection formation;

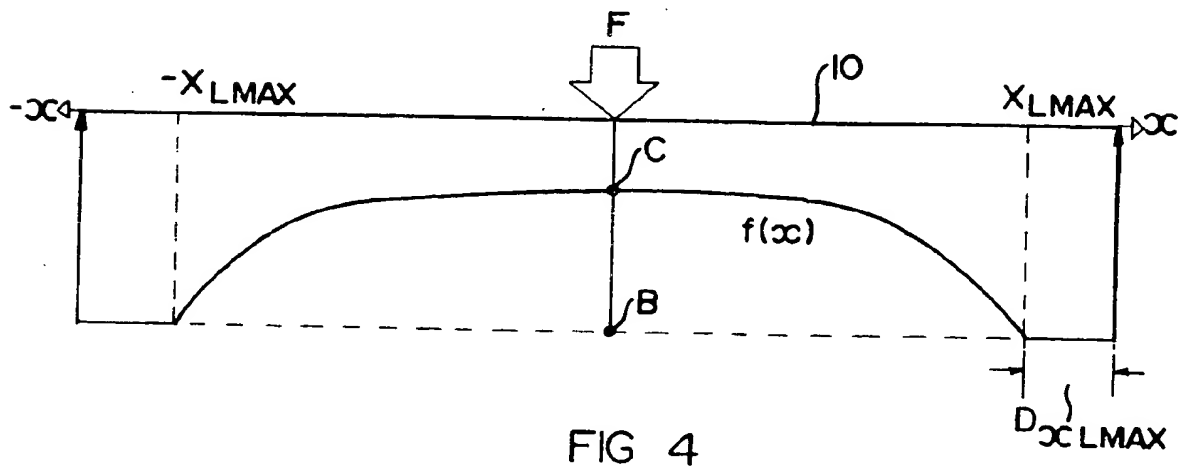
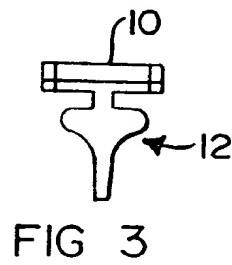
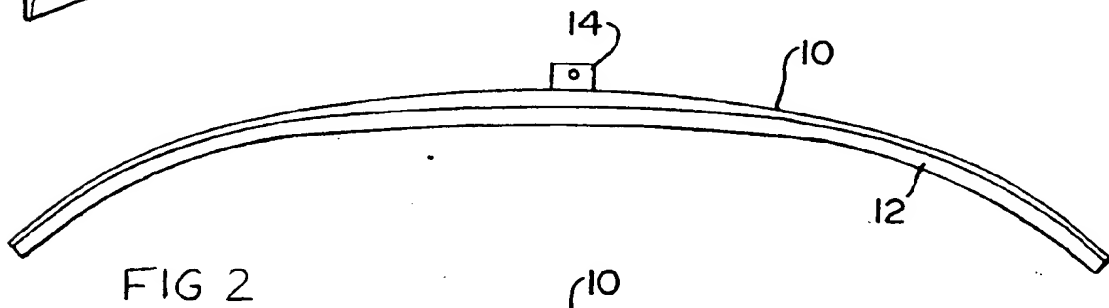
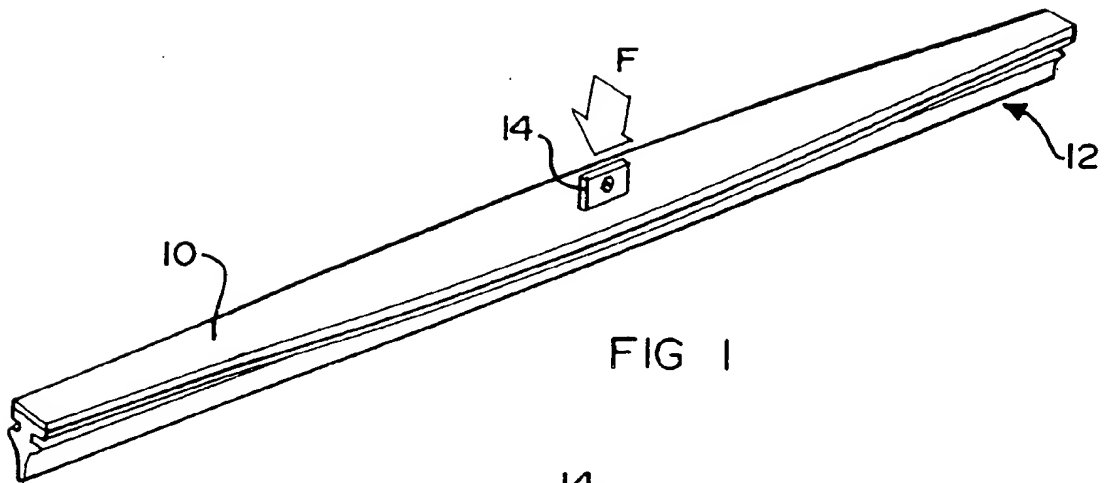
$h_x$  = thickness at  $x$ ;

$R_x$  = free-form radius of curvature of the backbone in the plane at  $x$ ;

$F$  = the total force applied to the said part of the backbone to straighten it against a flat surface;

$L$  = the length of said part; and

$E$  = modulus of elasticity.



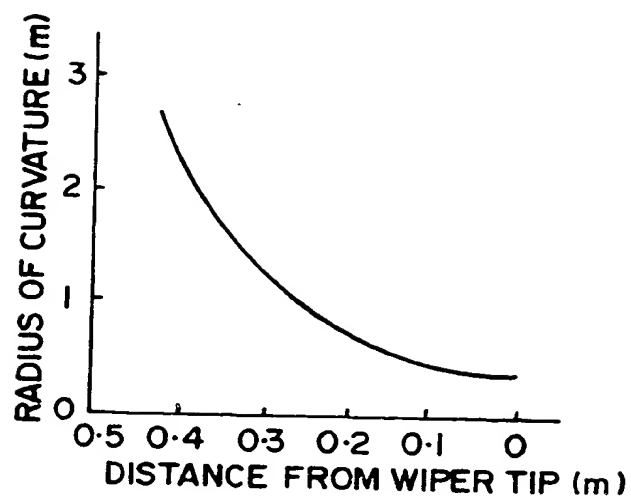


FIG 5

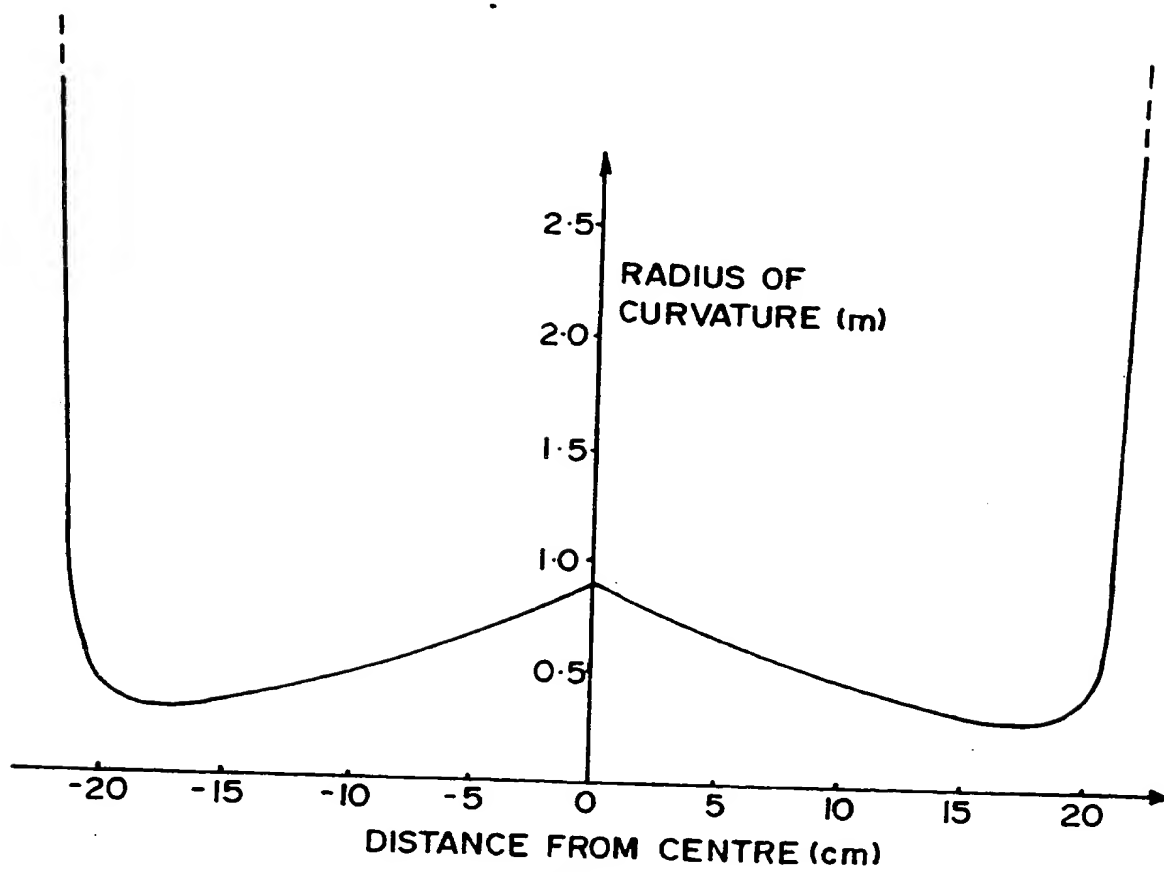


FIG 6

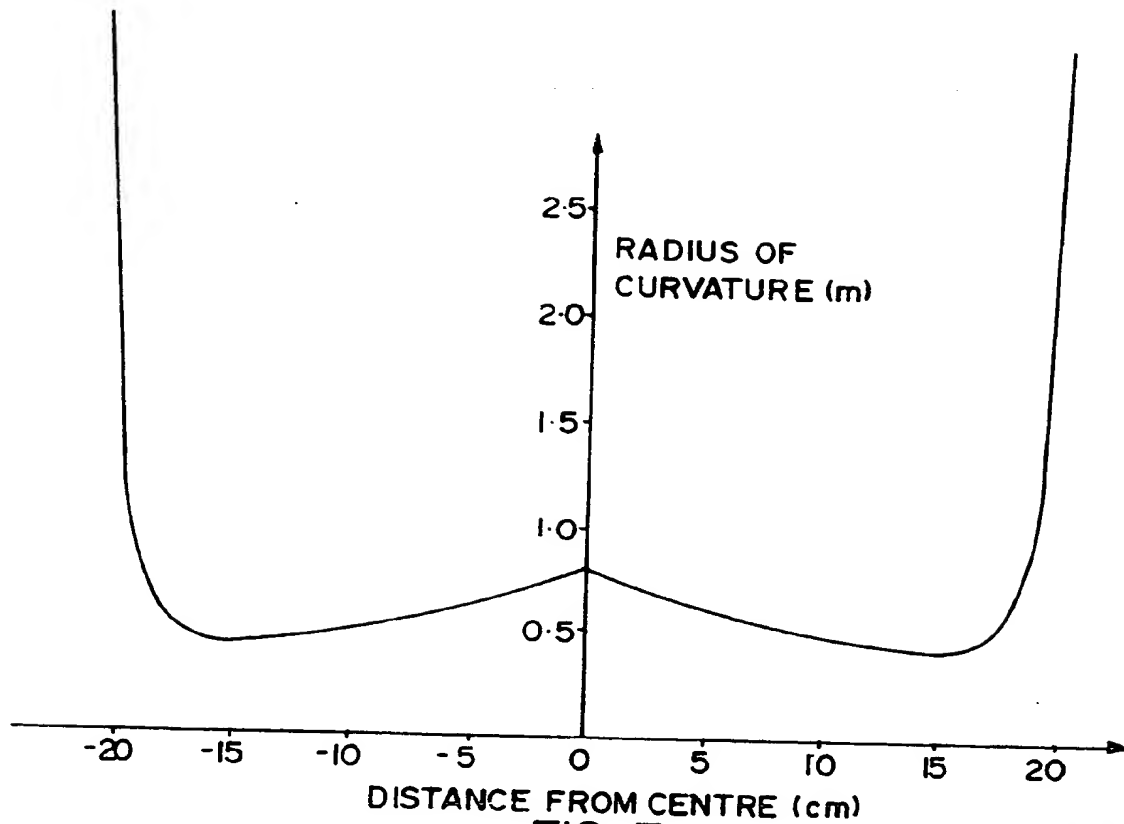


FIG 7

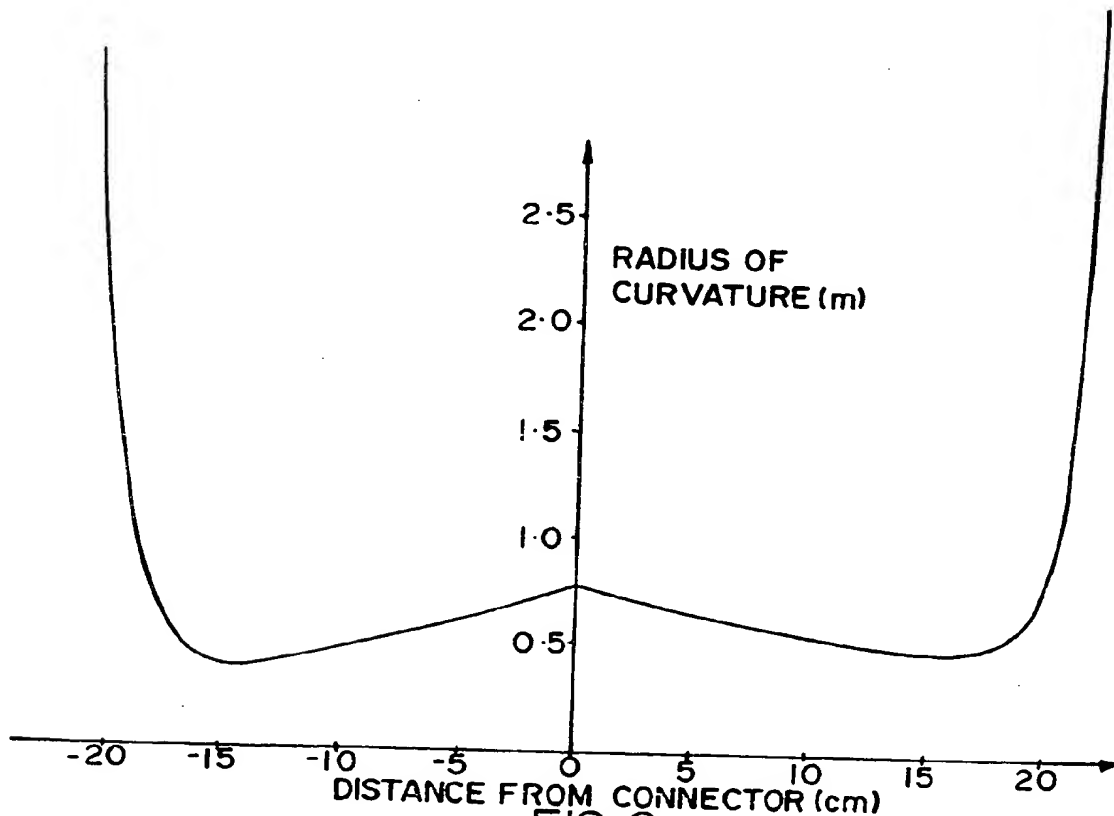


FIG 8



European Patent  
Office

# EUROPEAN SEARCH REPORT

Application Number

EP 92 30 7416

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl.5)
A	GB-A-1 012 902 (APPEL) * the whole document *	1-4, 21 22	B60S1/38
A	US-A-4 343 063 (BATT) * abstract; claims 1-7; figures 1, 2, 4-7, 9-11 * * column 2, line 36 - line 57 * * column 3, line 27 - column 5, line 12 *	1-5, 7, 8 21, 22	
A	US-A-3 480 986 (FORSTER) * the whole document *	1-4, 6, 21 22	
A	FR-A-2 515 121 (ROBERT BOSCH) * figures * * page 1, line 19 - page 2, line 22 * * page 4, line 27 - page 6, line 11 *	1-4, 6, 21 22	
			TECHNICAL FIELDS SEARCHED (Int. Cl.5)
			B60S
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 03 NOVEMBER 1992	Examiner WESTLAND P.G.
<p><b>CATEGORY OF CITED DOCUMENTS</b></p> <p>X : particularly relevant if taken alone  Y : particularly relevant if combined with another document of the same category  A : technological background  O : non-written disclosure  P : intermediate document</p> <p>T : theory or principle underlying the invention  E : earlier patent document, but published on, or after the filing date  D : document cited in the application  L : document cited for other reasons</p> <p>&amp; : number of the same patent family, corresponding document</p>			

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